

# ChemSet™ 801 Xtrem™ XC<sup>2</sup>

## CHEMICAL INJECTION - NON-CRACKED & CRACKED CONCRETE

### GENERAL INFORMATION

Performance Related	Installation Related

#### Product

Chemset™ 801 Xtrem™ XC<sup>2</sup> is a heavy duty Vinylester for anchoring threaded studs and reinforcing bar into cracked and uncracked concrete.

#### Compliance

European Technical Assessment (option 1) - ETA-18/0045

Design according to:

- AS5216 (formerly TS101)
- EN1992-4 (formerly ETAG001 Annex C, E & TR045)
- Use enclosed data for simplified calculation method

Use Ramset™ iExpert Anchor Software for optimised calculation or where a greater range of anchor layout detail is needed.

#### Benefits, Advantages and Features

- 50 year working Life
- Flooded Holes
- Fire rated

#### Greater productivity:

- Easy dispensing even in cold weather
- Apply torque in 2 hours @ 20°C

#### Greater security:

- Strong bond
- Rated for sustained loading

#### Versatile:

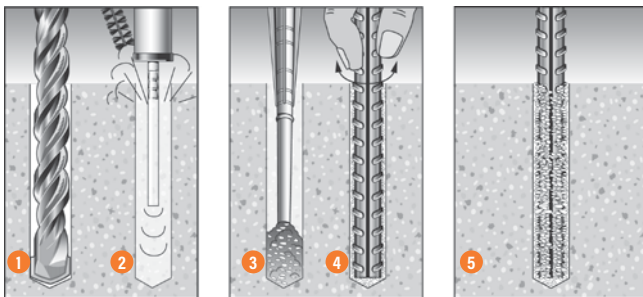
- Earthquake, Fire & Flooded Conditions
- Cold and temperate climates

#### Greater safety:

- Low odour
- Suitable for contact with drinking water
- VOC Compliant

Made in Australia

#### Installation



1. Drill or core hole to specified diameter and depth
2. **Important:** Use Ramset™ Dustless Drilling System to ensure holes are clean. Alternatively, clean dust and debris from hole with stiff wire or nylon brush and blower in the following sequence: blow x 2, brush x 2, blow x 2.
3. Screw mixing nozzle onto cartridge and dispense 2-3 trigger pulls of adhesive to waste until colour is grey with no streaks
4. Insert tip of nozzle to bottom of hole and dispense adhesive
5. Fill hole to about 2/3 full
6. Insert reinforcing bar with rotating motion to release trapped air
7. Wait until adhesive has fully cured before loading (see Working Time / Loading Time chart)
8. Clean up with Acetone



#### Principal Applications

- Threaded Studs
- Starter Bars
- Threaded Inserts
- Over-head installation
- Steel Columns
- Hand Rails
- Road Stitching

#### Recommended Installation Temperatures

	Minimum	Maximum
Substrate	5°C	40°C
Adhesive	5°C	40°C

#### Service Temperature Limits

-40°C to 80°C

#### Setting Times

Temperature of base material	Gel Time	Curing time in dry concrete	Curing time in wet concrete
+5°C	60 min	240 min	480 min
6°C - 10°C	40 min	180 min	360 min
11°C - 20°C	15 min	120 min	240 min
21°C - 30°C	8 min	90 min	180 min
31°C - 40°C	4 min	60 min	120 min

Note: Cartridge temperature minimum +5°C

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## CHEMICAL INJECTION - NON-CRACKED & CRACKED CONCRETE

Chemical Anchoring - Reinforcing Bar Anchorage

### Installation and performance details: ChemSet™ 801 Xtrem™ XC<sup>2</sup> and Reinforcing Bar

Anchor Size, d <sub>a</sub> (mm)	Drilled Hole diam., d <sub>h</sub> (mm)	Anchor Effective Depth, h (mm)	Optimum dimensions*			Reduced Characteristic Capacity #				
			Edge* distance, e <sub>c</sub> (mm)	Anchor spacing, a <sub>c</sub> (mm)	Concrete substrate thickness, b <sub>m</sub> (mm)	Gr 500 Rebar - Steel		Non-Cracked Concrete		
						Tension, φN <sub>us</sub> (kN)***	Shear, φV <sub>us</sub> (kN)	Tension, φN <sub>uc</sub> (kN)**		
								Concrete compressive strength, f' <sub>c</sub>		
20 MPa	32 MPa	40 MPa								
10	12	90	135	270	115	31.4	21.4	24.5	25.5	26.2
12	15	110	165	330	140	45.2	30.8	35.9	37.4	38.5
16	20	125	187	375	160	80.4	54.8	54.5	56.6	58.3
20	25	150	225	450	190	125.6	85.7	60.2	76.2	85.4
		170	255	510	215			72.6	91.9	99.1

\* Note: For shear loads acting towards an edge or where these optimum dimensions are not achievable, please use the simplified strength limit state design process to verify capacity.

\*\*Note: Reduced characteristic ultimate concrete tensile capacity = φN<sub>uc</sub> where φ = 0.67 and N<sub>uc</sub> = Characteristic ultimate concrete tensile capacity.

For conversion to Working Load Limit MULTIPLY φN<sub>uc</sub> x 0.5

\*\*\*Note: Reduced characteristic ultimate steel tensile capacity = φN<sub>us</sub> where φ = 0.8 and N<sub>us</sub> = Characteristic ultimate steel tensile capacity .

For conversion to Working Load Limit MULTIPLY φN<sub>us</sub> x 0.56

#Note: Design Tensile Capacity φN<sub>ur</sub> = minimum of φN<sub>uc</sub> and φN<sub>us</sub>

For Cracked Concrete performance, please use the simplified strength limit state design process to verify capacity.

Data is based on a Service temperature limit of -40°C to +40°C

Flooded Holes: Multiply φNuc x 0.75

For optimised performance data, please use Ramset iExpert Anchoring Software.

### DESCRIPTION AND PART NUMBERS

Description	Cartridge Size	Part No.
ChemSet™ 801 Xtrem™	750 ml	C801X750 (AU & NZ)
ChemSet™ 801 Xtrem™	380 ml	C801X380 (AU only)

Drilled hole depth, h1 (mm) h1 = h h = Effective depth	Substrate thickness b <sub>m</sub> (mm)				
	Anchor Stud Size (mm)				
	10	12	16	20	24
	h + 30mm ≥ 100mm			h + (2 x d <sub>a</sub> )	

### Typical Engineering Properties of Grade 500 Reinforcing Bar

Rebar Size	10	12	16	20
Drilled Hole Dia, d <sub>h</sub> (mm)	12	15	20	25
Stress Area, A <sub>s</sub> (mm <sup>2</sup> )	78.5	113	201	314
Yield Stress, f <sub>sy</sub> (MPa)	500	500	500	500
Tensile Steel Yield Capacity, N <sub>sy</sub> (kN)	39.3	56.5	100.5	157.0

For further information refer to reinforcing bar manufacturer's published information and current revision of AS/NZS 4671

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## STRENGTH LIMIT STATE DESIGN

### STEP 1

#### Select anchor to be evaluated

Table 1a Indicative combined loading - interaction diagram

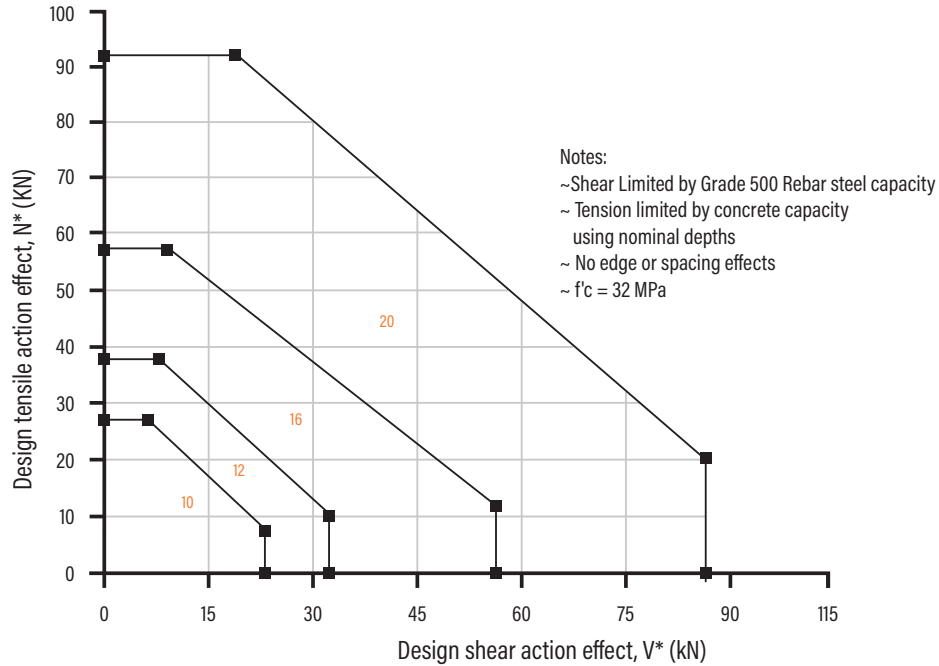


Table 1b Absolute minimum edge distance and anchor spacing values, e<sub>m</sub> and a<sub>m</sub> (mm)

Rebar size, d <sub>b</sub>	10	12	16	20
Min. Anchor Spacing - a <sub>m</sub>	50	60	80	100
Min. Edge Distance - e <sub>m</sub>	45	45	50	65

#### Step 1c Calculate anchor effective depth, h (mm)

Refer to nominal recommended effective depths, h, listed in installation and performance details table on previous page.

<p>Effective depth, h (mm)</p> <p>Preferred <math>h = h_n</math> otherwise,</p> <p><math>h = L_e - t</math></p> <p>t = total thickness of material(s) being fastened.</p>	Substrate thickness b <sub>m</sub> (mm)			
	Anchor Stud Size (mm)			
	10	12	16	20
	h + 30mm ≥ 100mm		h + (2 x d <sub>b</sub> )	

### Checkpoint 1

Anchor size determined, absolute minima compliance achieved, effective depth (h) calculated.

# ChemSet™ 801 Xtrem™ XC<sup>2</sup>

## STRENGTH LIMIT STATE DESIGN

Chemical Anchoring - Reinforcing Bar Anchorage

### STEP 2 Verify concrete tensile capacity - per anchor

Table 2a Reduced characteristic ultimate concrete tensile capacity,  $\phi N_{uc}$  (kN),  $\phi_c = 1/1.5 = 0.67$ ,  $f'_c = 32$  MPa

Rebar Size, $d_b$	Combined pull-out and concrete cone resistance - $\phi N_{ucp}$				Concrete Cone Resistance - $\phi N_{ucc}$
	10	12	16	20	
Drilled Hole Dia, $d_h$ (mm)	12	15	20	25	
Effective Depth, $h$ (mm)					
70	19.8				24.3
80	22.7				29.7
90	<b>25.5</b>	30.6			35.4
100	28.3	34.0			41.5
110	31.1	<b>37.4</b>			47.9
120	34.0	40.8	54.4		54.5
125	35.4	42.5	<b>56.6</b>		58.0
140	39.6	47.6	63.4		68.7
150	42.5	51.0	68.0	84.9	76.2
160	45.3	54.4	72.5	90.6	84.0
170	48.1	57.8	77.0	<b>96.3</b>	91.9
180	51.0	61.2	81.6	101.9	100.2
190	53.8	64.6	86.1	107.6	108.6
200	56.6	68.0	90.6	113.3	117.3
210		71.4	95.1	118.9	126.2
240		81.6	108.7	135.9	154.2
270			122.3	152.9	184.0
280			126.9	158.6	194.4
300			135.9	169.9	215.6
320			145.0	181.2	237.5
350				198.2	271.6
400				226.5	331.9

For optimised performance data, please use Ramset iExpert Anchoring Software.

Table 2a-2 Cracked Concrete effect, tension,  $X_{ncr}$

Rebar Size, $d_b$	Cracked Concrete Effect - $X_{ncr}$				$X_{ncr}$
	where $\phi N_{uc} = \phi N_{ucp}$ (from Table 2a)				
f'c (MPa)					where $\phi N_{uc} = \phi N_{ucc}$ (from Table 2a)
20 to 50	0.38	0.42	0.42	0.46	0.70

Bold values are at Chemset Anchor Stud nominal Depths

Flooded Holes: Multiply  $\phi N_{uc}$  x 0.75

For Sustained Loads MULTIPLY  $\phi N_{uc}$  x 0.6

For Non-cracked concrete  $X_{ncr} = 1$ .

Note: The maximum embedment depth shall be reduced to  $12d_b$  for installation in flooded holes

If concrete condition is Non-Cracked then, Refer to Checkpoint 2	If concrete condition is Cracked then, $\phi N_{uc} = \phi N_{ucp}$
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Table 2b-1 Concrete service temperature limits effect, tension,  $X_{nts}$

Rebar Size, $d_b$	Service temperature limits effect, tension, $X_{nts}$				$X_{nts}$
	where $\phi N_{uc} = \phi N_{ucp}$ (from Table 2a)				
Service temperature (°C)	10	12	16	20	where $\phi N_{uc} = \phi N_{ucc}$ (from Table 2a)
-40 °C to +40 °C			1.00		1.00
-40 °C to +80 °C			0.92		1.00

Table 2b-2 Concrete compressive strength effect, tension,  $X_{nc}$

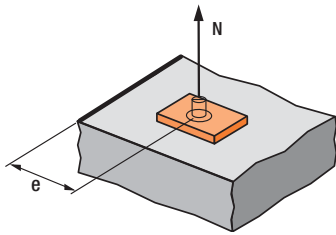
NON- CRACKED	Non-Cracked Concrete - $X_{nc}$				$X_{nc}$
	where $\phi N_{uc} = \phi N_{ucp}$ (from Table 2a)				
Rebar Size, $d_b$	10	12	16	20	where $\phi N_{uc} = \phi N_{ucc}$ (from Table 2a)
f'c (MPa)					
20	0.96	0.96	0.96	0.96	0.79
25	0.96	0.96	0.96	0.96	0.88
32	1.00	1.00	1.00	1.00	1.00
40	1.03	1.03	1.03	1.03	1.12
50	1.05	1.05	1.05	1.05	1.25

CRACKED	Cracked Concrete - $X_{nc}$				$X_{nc}$
	where $\phi N_{uc} = \phi N_{ucp}$ (from Table 2a)				
Rebar Size, $d_b$	10	12	16	20	where $\phi N_{uc} = \phi N_{ucc}$ (from Table 2a)
f'c (MPa)					
20 - 50	0.96	0.96	0.96	0.96	0.79

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## STRENGTH LIMIT STATE DESIGN



$$X_{ne} = 0.25 + 0.5 \cdot (e/h)$$

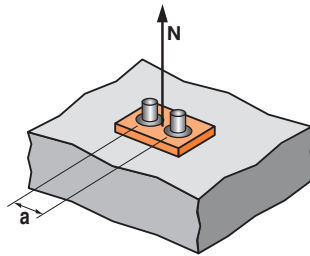
Where  $e_m \leq e \leq e_c$

$$e_c = 1.5 \cdot h$$

Note: Tabled values are based on the nominal effective depth,  $h$  shown in the installation details. For other values of  $X_{ne}$ , please use equation shown above.

Table 2c - Concrete Edge distance effect, tension,  $X_{ne}$

Anchor size, $d_b$	10	12	16	20
Edge distance, $e$ (mm)				
45	0.50	0.45		
50	0.53	0.48	0.45	
65	0.61	0.55	0.51	0.44
85	0.72	0.64	0.59	0.50
90	0.75	0.66	0.61	0.51
100	0.81	0.70	0.65	0.54
120	0.92	0.80	0.73	0.60
135	1	0.86	0.79	0.65
165		1	0.91	0.74
187			1	0.80
255				1



$$X_{na} = 0.5 + a/(6 \cdot h)$$

Where  $a_m \leq a \leq a_c$

$$a_c = 3 \cdot h$$

Note: Tabled values are based on the nominal effective depth,  $h$  shown in the installation details. For other values  $X_{na}$ , please use equation shown above.

Table 2d - Concrete anchor spacing effect, tension,  $X_{na}$

Anchor size, $d_b$	10	12	16	20
Anchor spacing, $a$ (mm)				
50	0.59			
60	0.61	0.59		
80	0.65	0.62	0.61	
100	0.69	0.65	0.63	0.60
120	0.72	0.68	0.66	0.62
150	0.78	0.73	0.70	0.65
200	0.87	0.80	0.77	0.70
270	1	0.91	0.86	0.76
330		1	0.94	0.82
375			1	0.87
510				1

**Checkpoint 2**

Design reduced ultimate concrete tensile capacity,  $\phi N_{urc}$

$$\phi N_{urc} = \phi N_{uc} \cdot X_{ncr} \cdot X_{ns} \cdot X_{nc} \cdot X_{ne} \cdot X_{na}$$

If concrete condition is Non-Cracked then

$$\phi N_{urc} = \text{minimum of } \phi N_{ucp} \cdot X_{ncr} \cdot X_{ns} \cdot X_{nc} \cdot X_{ne} \cdot X_{na} \text{ and } \phi N_{ucc} \cdot X_{ncr} \cdot X_{ns} \cdot X_{nc} \cdot X_{ne} \cdot X_{na}$$

**STEP 3**

**Checkpoint 3**

### Verify anchor tensile capacity - per anchor

Table 3a Reduced characteristic ultimate steel tensile capacity,  $\phi N_{us}$  (kN), where  $\phi = 0.8$

Anchor size, $d_b$	10	12	16	20
Gr 500 Rebar	31.4	45.2	80.4	125.6

Design reduced ultimate tensile capacity,  $\phi N_{ur}$

$$\phi N_{ur} = \text{minimum of } \phi N_{urc}, \phi N_{us}$$

Check  $N^*/\phi N_{ur} \leq 1.0$ ,

if not satisfied return to step 1

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## STRENGTH LIMIT STATE DESIGN

Chemical Anchoring - Reinforcing Bar Anchorage

### STEP 4

#### Step 4 - Verify Concrete Shear Capacity - per anchor

Table 4a-1 Reduced characteristic ultimate concrete edge shear capacity,  $\phi V_{uc}$  (kN),  $\phi = 1/1.5 = 0.67$ ,  $f'_c = 32$  MPa

Rebar size, $d_b$	10	12	16	20
Effective depth, $h$ (mm)	70 - 200	90 - 240	120 - 320	150 - 400
Edge distance, $e_m$				
45	5.0	5.5		
50			7.2	
65				11.1

For optimised performance data, please use Ramset iExpert Anchoring Software.

Table 4a-2 Cracked Concrete effect, shear,  $X_{vcr}$

Anchor size, $d_b$	10	12	16	20
$X_{vcr}$	0.70			

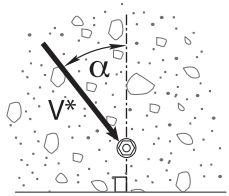
For Non-cracked concrete  $X_{vcr} = 1.0$

Table 4b - Concrete compressive strength effect, shear,  $X_{vc}$

$f'_c$ (MPa)	20	25	32	40	50
$X_{vc}$	0.79	0.86	1.0	1.11	1.22

Table 4c - Concrete load direction effect, concrete edge shear,  $X_{vd}$

Angle, $\alpha^\circ$	0-55	60	70	80	90-180
$X_{vd}$	1	1.1	1.2	1.5	2

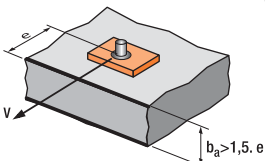


Load direction effect, conc. edge shear,  $X_{vd}$

Table 4d - Concrete anchor spacing and edge distance effect, concrete edge shear,  $X_{ve}$

For single anchor fastening  $X_{ve}$

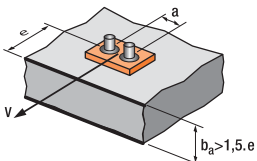
$e/e_m$	1.0	1.2	1.4	1.6	1.8	2.0	2.2	2.4	2.6	2.8	3.0	3.2
$X_{ve}$	1.00	1.31	1.66	2.02	2.41	2.83	3.26	3.72	4.19	4.69	5.20	5.72



$$X_{ve} = e/e_m * \sqrt{e/e_m}$$

For 2 anchors fastening  $X_{ve}$

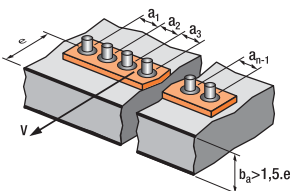
$e/e_m$	1.0	1.2	1.4	1.6	1.8	2.0	2.2	2.4	2.6	2.8	3.0	3.2
$a/e_m$												
1.0	0.67	0.84	1.03	1.22	1.43	1.65	1.88	2.12	2.36	2.62	2.89	3.16
1.5	0.75	0.93	1.12	1.33	1.54	1.77	2.00	2.25	2.50	2.76	3.03	3.31
2.0	0.83	1.02	1.22	1.43	1.65	1.89	2.12	2.38	2.63	2.90	3.18	3.46
2.5	0.92	1.11	1.32	1.54	1.77	2.00	2.25	2.50	2.77	3.04	3.32	3.61
3.0	1.00	1.20	1.42	1.64	1.88	2.12	2.37	2.63	2.90	3.18	3.46	3.76
3.5		1.30	1.52	1.75	1.99	2.24	2.50	2.76	3.04	3.32	3.61	3.91
4.0			1.62	1.86	2.10	2.36	2.62	2.89	3.17	3.46	3.75	4.05
4.5				1.96	2.21	2.47	2.74	3.02	3.31	3.60	3.90	4.20
5.0					2.33	2.59	2.87	3.15	3.44	3.74	4.04	4.35
5.5						2.71	2.99	3.28	3.71	4.02	4.33	4.65
6.0							2.83	3.11	3.41	3.71	4.02	4.33



$$X_{ve} = \frac{3*e+a}{6*e_m} * \sqrt{e/e_m}$$

For 3 anchors fastening and more

$$X_{ve} = \frac{3*e + a_1 + a_2 + a_3 + \dots + a_{n-1}}{3*n*e_m} * \sqrt{e/e_m}$$



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## STRENGTH LIMIT STATE DESIGN

Table 4e Reduced characteristic ultimate concrete pryout capacity,  $\phi V_{ucp}$  (kN),  $\phi = 1/1.5 = 0.67$ ,  $f'_c = 32$  MPa

Rebar size, $d_b$	10	12	16	20
Effective depth, $h$ (mm)	90	110	125	170
-40 °C to +40 °C	51.0	74.8	158.6	192.6
-40 °C to +80 °C	47.0	69.0	104.6	177.7

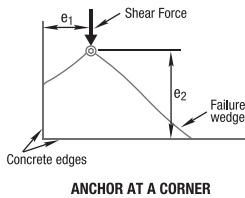


Table 4f Anchor at a corner effect, concrete edge shear,  $X_{vs}$

Note: For  $e_1/e_2 > 1.25$ ,  $X_{vs} = 1.0$

Edge distance, $e_2$ (mm)	25	30	35	50	60	75	125	200	300	400	600	900
Edge distance, $e_1$ (mm)												
25	0.86	0.77	0.70	0.58	0.53	0.49	0.41	0.37	0.35	0.34	0.32	0.32
30	0.97	0.86	0.78	0.64	0.58	0.52	0.43	0.38	0.36	0.34	0.33	0.32
35	1.00	0.95	0.86	0.69	0.63	0.56	0.46	0.40	0.37	0.35	0.33	0.32
50	1.00	1.00	1.00	0.86	0.77	0.67	0.52	0.44	0.39	0.37	0.35	0.33
60	1.00	1.00	1.00	0.97	0.86	0.75	0.57	0.47	0.41	0.38	0.36	0.34
75	1.00	1.00	1.00	1.00	1.00	0.86	0.64	0.51	0.44	0.41	0.37	0.35
125	1.00	1.00	1.00	1.00	1.00	1.00	0.86	0.65	0.53	0.48	0.42	0.38
200	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.86	0.67	0.58	0.49	0.42
300	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.86	0.72	0.58	0.49
400	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.86	0.67	0.55
500	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.77	0.61
600	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.86	0.67
900	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.86

Checkpoint **4a**

Design reduced ultimate concrete edge shear capacity,  $\phi V_{urc}$

$$\phi V_{urc} = \phi V_{uc} * X_{vcr} * X_{vc} * X_{vd} * X_{ve} * X_{vs}$$

Checkpoint **4b**

Design reduced ultimate concrete pryout capacity,  $\phi V_{urcp}$

$$\phi V_{urcp} = \phi V_{ucp} * X_{ncr} * X_{nc} * X_{ne} * X_{na}$$

STEP **5**

Verify anchor shear capacity - per anchor

Table 5a Reduced characteristic ultimate steel shear capacity,  $\phi V_{usr}$  (kN) where  $\phi_v = 0.8$

Anchor size, $d_b$	10	12	16	20
Gr 500 Rebar	21.4	30.8	54.8	85.7

Checkpoint **5**

Design reduced ultimate shear capacity,  $\phi V_{ur}$

$$\phi V_{ur} = \text{minimum of } \phi V_{urc}, \phi V_{urcp}, \phi V_{usr}$$

Check  $V^*/\phi V_{ur} \leq 1$ ,

if not satisfied return to step 1

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## STRENGTH LIMIT STATE DESIGN

### STEP 6 Combined loading and specification

#### Checkpoint 6

Check

$N^*/\phi N_{ur} + V^*/\phi V_{ur} \leq 1.2,$   
if not satisfied return to step 1

#### Specify - Reinforcing Bar Anchorage

Ramset 801 Xtrem™ XC<sup>2</sup> Injection (Anchor Size) grade 500 Rebar.  
Drilled hole depth to be (h) mm.

#### Example

Ramset 801 Xtrem™ XC<sup>2</sup> Injection with  
20mm grade 500 Rebar  
Drilled hole depth to be 125 mm.  
To be installed in accordance with  
Ramset Installation Instructions.

Ramset™ iExpert Anchor Software for optimised calculation or where a greater range of anchor layout detail is needed.